Appendix E

Air Quality Analysis

This appendix provides information to support the non-radiological air quality impact analysis presented in Section 5.2. This analysis characterizes the routine emission of non-radiological pollutants by most Hanford Solid Waste Program activities, the atmospheric dispersion of these pollutants, and the maximum air quality impacts to the public. The impacts associated with waste transportation activities and the emission of hazardous chemicals and radionuclides are not addressed in Section 5.2 or this appendix. Section 5.8 covers the air quality impacts associated with the transportation of radioactive and hazardous wastes. Section 5.11 and Appendix F report on the potential health impacts associated with the emission of chemicals and radionuclides.

The Clean Air Act authorizes the U.S. Environmental Protection Agency (EPA) to set permissible levels of exposure for selected air pollutants using health-based criteria. These "criteria pollutants" include nitrogen dioxide (NO₂), sulfur dioxide (SO₂), particulate matter with aerodynamic diameters of 10 microns or less (PM₁₀), carbon monoxide (CO), lead, and ozone. The maximum permissible exposure levels for these pollutants are set in National Primary and Secondary Ambient Air Quality Standards (40 CFR 50). The standards focus on short-term exposures (1 hr or 3 hr), workday exposures (8 hr), and long-term exposures (24 hr or annual). The standards for some pollutants focus on short-term exposures (for example, CO and ozone), and the standards for other pollutants focus on long-term exposures (for example, PM₁₀ and NO₂). Primary standards are established to protect against adverse health effects. Secondary standards protect the public welfare from negative effects such as damage to crops, vegetation, and buildings, as well as decreased visibility. In addition, states and local governments can set additional or more restrictive standards. Washington State has defined such standards for particulate matter and sulfur dioxide. Section 4.2.3 indicates the standards applicable to the Hanford Site.

Carbon monoxide, particulate matter, sulfur dioxide, and nitrogen dioxide are produced from the combustion of fossil fuels. Particulate matter is generated also by the mechanical disturbance of ground materials by earthmoving activities, vehicle traffic over unpaved and paved roadways, and the action of the wind on disturbed soils. Two criteria pollutants, ozone^(a) and lead, are not considered in this assessment because the level of their emissions, or that of essential precursor compounds, is negligible.

To estimate maximum air quality impacts from Hanford Solid Waste Program activities, the Industrial Source Complex Short-Term (ISCST3) Dispersion Model (EPA 1995b) was selected for use.

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⁽a) Volatile organic compounds (VOCs), a class of pollutant involved in ozone formation, would have a maximum project emission rate of less than 1 g/s. This release rate would not cause a detectable change in background concentration of this class of pollutants and therefore could not result in any detectable change in ozone concentrations within the local airshed.

The ISCST3 model is approved by the EPA for the calculation of the maximum air quality impacts of criteria pollutants. The model uses a steady-state Gaussian plume algorithm to estimate pollutant concentrations from a wide variety of sources associated with industrial complexes. The model is applicable for either flat or rolling terrain, modeling domains with a radius of 50 km (31 mi) or less from the point of release, and urban or rural environments.

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Multiple years of hourly meteorological data from the Hanford Site were used in conducting ISCST3 modeling. These data provided an extended, climatologically representative period of local meteorology for computing atmospheric dispersion conditions. The hourly meteorological data covered a representative 4-yr period (1993 through 1996) and included such parameters as wind transport direction, wind speed, atmospheric stability, mixing depth, and air temperature. All meteorological data were obtained from the Hanford Meteorology Station (HMS). The HMS is located between the 200 West and 200 East Areas; data from this station are representative of meteorological conditions at the Hanford Solid Waste Program work sites in and around the 200 Areas. Area C is located about 6 km (4 mi) south of the HMS and data from the station are also representative of meteorological conditions at this work site. Wind measurements were made at 10 m (33 ft) above ground level on the 122-m (400-ft) tall instrumented tower located adjacent to the HMS. Wind transport directions were reported in the data set using 36 direction sectors (i.e., the sectors are 10 degrees wide). Near-surface air temperature measurements were made at 1.5 m (5 ft) above ground level. Mixing-depth estimates were made using measurements from the HMS Doppler acoustic sodar, the HMS instrumented tower, and other sources of information. Atmospheric stability was computed using the U.S. Nuclear Regulatory Commission (NRC) ?T method (NRC 1972). This methodology uses the wind speed and the difference between temperature measurements at 60 m (200 ft) and 10 m (30 ft) above the ground to estimate the atmospheric stability class.

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The ISCST3 model uses meteorological data records to compute the maximum air quality impacts for various federal- and state-defined averaging periods and receptor locations. A Cartesian grid, polar grid, and an array of user-defined receptor points were all used in modeling air quality impacts. This dense network of receptors was used to capture air quality impacts to the public along the Hanford Site boundary, outside the boundary, and at points of public access within the boundaries of the site.

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The characterization of pollutant emissions from Hanford Solid Waste Program activities was a critical step in the air quality analysis. Criteria pollutant emissions would come from fugitive dust sources, diesel-fueled engines, and propane-fired equipment. The operation of vehicles and construction equipment would generate both exhaust and fugitive dust emissions. Major pollutant generating activities would include:

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- construction or modification of waste-processing facilities (e.g., T Plant, CWC)
- construction of waste-disposal trenches (e.g., LLW, MLLW, ILAW)
 - waste-disposal operations
 - excavation of backfill and capping material at the borrow pits
- transportation of capping materials from the borrow pit area to the disposal trenches
- backfill and capping activities at the disposal trenches
 - leachate drying operations.

To simplify the modeling of air quality impacts, emissions from Hanford Solid Waste Program activities were conservatively assumed to originate from only three source locations. These source locations were situated in the 200 West Area (near the southwestern edge of local project activities), 200 East Area (near the northwestern edge of local project activities), and Area C (at the borrow pit work site near State Route [SR] 240). These source locations were chosen because they represented the project work site in their major operating area that would generate the greatest air quality impacts to the public.

The 200 Area source locations were each represented using a 40 m by 40 m (130 ft by 130 ft) emissions area. The Area C source location was represented using two 40 m by 40 m emission areas. The emission area used to represent borrow pit operations was set on the southwest side of SR 240. The Area C emissions used to represent truck-loading operations was set on the northeast side of the highway. Both emissions areas were conservatively positioned so that they extend between 150 m (490 ft) and 95 m (310 ft) from SR 240. This is less than the 150-m minimum distance specified in project guidelines for conducting activities near SR 240. During Area C operations, most emissions would actually occur at distances between 300 m (980 ft) and 1.6 km (1 mile) from the highway. In modeling emissions from borrow pit operations, 4 diesel-powered vehicles (a scraper, bulldozer, front-end loader, and track hoe) were assumed to be operating at the borrow pit source location. In addition to the diesel exhaust, fugitive dust emissions from equipment operations and the material stockpile were also included in the source term. Detailed information on borrow pit operations is provided in FH (2002).

The coordinates and sizes of all source locations were selected to provide conservative estimates of the maximum potential air quality impacts to the public that would result from activities to be conducted within each area. This included concentrating emissions from multiple activities into one source location, even though these emissions would actually occur at multiple work sites spread over a much larger work area. The transportation of backfill and capping materials was also handled in this manner. Twenty diesel-powered trucks were assumed to be in continuous operation during normal work periods to facilitate the transportation of the materials from Area C to the 200 Areas. Pollutant emissions associated with the operation of the trucks include exhaust emissions and fugitive dust. A conservative assumption was made that all truck emissions would be split between two fixed source locations: Area C and the 200 West Area. This assumption concentrated emissions rather than spreading them across a much broader area or line source, thereby maximizing estimates of air quality impacts.

Another conservative assumption involved not accounting for processes that would chemically decompose pollutants or remove pollutants from the atmosphere via deposition processes. In actuality, chemical decomposition and atmospheric-deposition processes would act to substantially reduce most pollutant concentrations and associated air quality impacts.

Based on ISCST3 model runs for pollutant releases in the 200 East and 200 West Areas, the locations where maximum air quality impacts to the public would occur were determined for various averaging periods. Table E.1 provides estimates of the maximum air quality impact locations and the associated dispersion factors. Multiplying a dispersion factor (s/m³) by a maximum pollutant release rate (μ g/s) generates an estimate of the maximum air-pollutant concentration (μ g/m³). For criteria pollutants with ambient air quality standards based on 8-hr or less averaging times, the maximum air quality impacts for emissions from the 200 Areas would occur at points of public access along SR 240. For criteria

pollutants with 24-hr and annual standards, the greatest air quality impacts would occur at the Site boundary, the closest point where a member of the public could potentially be located for an extended period of time. Long-term air quality impacts are not computed for SR 240 because this highway passes through federal lands with restricted public access (between the Hanford Site and the Fitzner/Eberhardt Arid Lands Ecology Reserve).

The 200 East and 200 West dispersion-factors indicate that for a unit emission, releases from the 200 West Area would have a slightly greater air quality impact than would emissions from the 200 East Area. As a result, for project activities that could occur in either the 200 East or 200 West Areas, the bounding 200 West dispersion factor was used to estimate air quality impacts. For example, the Lined Modular Facility proposed in Alternative Group D could be sited at locations in or near the 200 East or 200 West Areas, depending on the sub-alternative selected. The 200 West source location was used in the air quality analysis because it generated the greatest air quality impacts.

Table E.1. 200 East and 200 West Area Emissions: Dispersion Factors Used to Determine Maximum Air Quality Impacts to the Public

Area	Averaging Time Period	Maximum Impact Location and Corresponding Public Access	Distance and Direction from Pollutant Release Location to Maximum Public Impact Location (a)	Dispersion Factor for Maximum Impact Location (s/m³) ^(b)
200	1 hr	SR 240	8.5 km – SW	8.4E-5
East	3 hr	SR 240	9.0 km – SSW	3.3E-5
	8 hr	SR 240	9.0 km – SSW	2.2E-5
	24 hr	Hanford Site boundary	15.3 km – WNW	9.3E-6
	Annual	Hanford Site boundary	13.9 km – WNW	8.9E-8
200	1 hr	SR 240	4.0 km – S	1.6E-4
West	3 hr	SR 240	4.0 km – S	7.4E-5
	8 hr	SR 240	4.0 km – S	5.1E-5
	24 hr	Hanford Site boundary	8.5 km – WNW	1.6E-5
	Annual	Hanford Site boundary	11.5 km – W	1.5E-7

⁽a) Distance and direction determined by dispersion modeling. Pollutant-transport direction is reported using 16 compass sectors—starting with North (N) and continuing clockwise with NNE, NE, ENE, E (East), ESE, SE, SSE, S (South), SSW, SW, WSW, W (West), WNW, NW, and NNW.

Table E.2 provides the locations where maximum air quality impacts to the public would occur for releases from the Area C borrow pit. The maximum short-term air quality impacts for emissions from the borrow pit would occur along SR 240, and the maximum long-term air quality impacts would occur at the Site boundary. These impact locations are different from those for 200 Areas.

Hanford Solid Waste Program activities that would be associated with criteria pollutant emissions are shown in the timeline of Tables E.3 through E.8. These timelines show the expected years of various activities. Figure E.1 precedes Tables E.3 through E.8 to provide a key for interpreting the timelines.

⁽b) Values computed by the ISCST3 model. To convert to a concentration estimate ($\mu g/m^3$), a dispersion factor (s/m³) is multiplied by the actual pollutant release rate ($\mu g/s$).

Averaging	Maximum Impact	Distance from Release to Maximum	Unit Dispersion Factors for Maximum
Time	Location	Public Impact Location ^(a)	Impact Location (s/m ³) ^(b)
1 hr	SR 240	<150 m NE	3.3E-3
3 hr	SR 240	<150 m NE	2.3E-3
8 hr	SR 240	<150 m NE	1.9E-3
24 hr	Hanford Site Boundary	14.4 km WNW	1.0E-5
Annual	Hanford Site Boundary	13.8 km WNW	9.2E-8

⁽a) Distance and direction determined by dispersion modeling. Pollutant-transport direction is reported using 16 compass sectors—starting with North (N) and continuing clockwise with NNE, NE, ENE, E (East), ESE, SE, SSE, S (South), SSW, SW, WSW, W (West), WNW, NW, and NNW.

⁽b) Values computed by the ISCST3 model. To convert to a concentration estimate ($\mu g/m^3$), the dispersion factor (s/m^3) is multiplied by the actual pollutant release rate ($\mu g/s$).

KEY to TIMELINE TABLES E.3-E.8

Column Headings: H=Hanford Only waste volume; L=Lower Bound waste volume; U = Upper Bound waste volume; and N = No Action waste volume that is disposed (as opposed to stored). N/A = activity is not applicable to the alternative; NWPF = new waste processing facility.

CONSTRUCTION

LLW Trench – Number indicates the number of low-level waste (LLW) trenches constructed during that year. The trench design can change by alternative. A fraction of a trench indicates that a less-than-full-sized trench, according to the design considered under the alternative, will be constructed.

MLLW Trench – Number indicates the number of mixed low-level waste (MLLW) trenches constructed during that year. The trench design can change by alternative. A fraction of a trench indicates that a less-than-full-sized trench, according to the design considered under the alternative, will be constructed. The "m" indicates the Phase I melter trench construction. "I" indicates ILAW trench (Alternative Groups A through E) or ILAW vault (No Action) construction. Six ILAW vaults are assumed to be constructed at a time.

CWC Bldgs – Number indicates the number of new Central Waste Complex (CWC) buildings to be constructed. Under the No Action Alternative, the first number indicates the number of CWC buildings constructed to store MLLW, and the second number indicates the number of CWC buildings constructed to store transuranic (TRU) waste. Also under the No Action Alternative, "melter pad construction" indicates the year that a pad would be constructed to store melters.

T Plant Modif – Construction activity associated with T-Plant modification for waste treatment occurs. **NWPF** – Construction of the new waste processing facility occurs.

LMF – Lined Modular Facility – also may be called the Lined Modular Trench

CAPPING

LLW – Check marks are the years that the LLW burial grounds will be capped.

MLLW – The number indicates the total number of MLLW trenches capped during that year. The first two trenches to be capped are the existing trenches (MLLW Trenches 31 and 34). The "m" indicates Phase I Melter trench capping. The "I" indicates ILAW trench or vault capping.

OTHER

CWC Propane – The amount of propane required to power vehicles for routine operations at CWC are indicated as increasing or decreasing over time.

MLLW Propane – The number indicates the number of MLLW trenches that require leachate processing by pulse driers.

Figure E.1. Information Key to the Timeline Tables (Tables E.3 - E.8)

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 Table E.8.
 Timeline of No Action Alternative Resulting in Criteria Pollutant Emissions

	I	CONSTRUCTION MILLW/						C	APPING	1	0'	THER	
			MLI	LW/	CONSTR	0011011		<u> </u>	MLI		Ŭ		
	Ll	LW	Mel		ILAW	CWC Bldgs	NWPF/T		melt		CWC		LLW
	Tre	ench	Tre		Vaults	LLW+MLLW/TRU	Plant	LLW	ILA	W	Propane	Pro	pane
	Н	N	N/A	N/A		H & N	N/A	N/A	H	N	H & N	H	N
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		_											
	3	3			*						ļ		
	1	1			I						I		
2005	1	1			T	4/3					N C		
2005	1	1			I I	4/3					R		
	2	2			1	4/3			1	1	E		
						4/3 &			1	1			
					I	melter pad					A		
	1	1			I	4/3					S		
2010	1	1			-	4/3			1	1	E		
	2	2			I	4/4		t			<u> </u>		
	2	2			I	4/4					O		
	2	2				4/4					P		
	2	2			I						S		
2015	1	1											
	3	3			I								
	2	2									▼		
					I				m	m	*		
	3	3									С		
2020	1	1			I						0		
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2025	0.3	0.3									N		
											Т	3	3
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2030									T	T	V	3	3
2030	0.3	0.3							I	I	E	3	3
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	1	}						-	I	I	ᆫ	3	3
	1	1						1	I	Ţ	0	3	3
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												0	0
2050													

E.1 Combustion Engine Emissions

For the facilities and operations evaluated in this study, diesel-fueled engines would be used in machines such as backhoes, forklifts, and air compressors. Propane fuel would be used in leachate-treatment equipment beginning in 2026 and for CWC vehicles. Gasoline would be used to fuel construction-support vehicles. However, these would generally be mobile sources and use very small quantities of fuel compared to the program's diesel-powered construction equipment. Therefore, criteria pollutant emissions from gasoline-fueled vehicles were not explicitly evaluated. Criteria pollutant emissions from diesel engines are estimated using the following equation:

$$A_{o, c, a} = F_{o, a} \times E_{c, f} \times D_{a}$$
 (E.1)

where $A_{o, c, a}$ = air concentration of criteria pollutant \mathbf{c} with an averaging time \mathbf{a} for operation \mathbf{o} $\mu g/m^3$

 $F_{o,a}$ = fuel-consumption rate for operation **o** and averaging time **a** L/s (or gal/s) $E_{c,f}$ = generation rate of criteria pollutant **c** for fuel **f** μ g/L (or μ g/gal)

 $D_a = \text{dispersion factor for averaging time } \mathbf{a}, \mu g/m^3 \text{ per g/s.}$

Dispersion factors (D_a) were given in Table E.1 and Table E.2. The generation rates for criteria pollutants ($E_{c,\,\theta}$) for diesel fuel and propane are shown in Table E.9. The rates of pollutant generation for diesel fuel for carbon monoxide, nitrogen dioxide, and particulates are based on average values for a variety of heavy-duty construction equipment (EPA 1991). The values for particulates listed in Table E.9 are total suspended particulates but are conservatively assumed to be PM_{10} . Sulfur dioxide emissions are based on the maximum permissible amount of sulfur allowed in diesel fuel (a 500-ppm limit). No credit is taken for the substantial reduction in the sulfur content of diesel fuel (a 15-ppm limit) scheduled to be phased in beginning in June 2006 or a tightening of the emission standards for nitrogen dioxide and particulate matter scheduled to be phased in beginning in 2007 (EPA 2000). The propane-pollutant generation rates presented in Table E.9 are based on a propane industrial boiler (EPA 1996).

Fine material on road surfaces is emitted into the atmosphere as a result of vehicular traffic. The rate of particulate emissions is a function of the weight and the amount of dust on the road surface. Equations for computing the rate of particulate emissions are provided by EPA (1988). Using information on the

Table E.9. Emission Factors for Criteria Pollutants

	Diesel-Fuel Pollutant Generation Rate	Propane Pollutant Generation Rate
Criteria Pollutant	(mg pollutant/L diesel fuel)	(mg pollutant/gal propane)
Carbon monoxide	1.5E+7	1.4E+6
Nitrogen dioxide	3.9E+7	8.6E+6
Particulates	3.5E+6	2.7E+5
Sulfur dioxide	8.2E+5	None

likely dust concentrations on paved roads at Hanford (0.4 g/m²) and the average weight of the trucks, a rate of PM_{10} emissions at 16 g (0.564 oz) per vehicle mile traveled was conservatively estimated. For a 24-km (15-mi) roundtrip, this equates to a PM_{10} emission rate of 0.067 g/s per truck.

1 2

Fuel consumption rates ($F_{o,a}$ of Equation E.1) are shown in Table E.10 for diesel fuel and Table E.11 for propane. The fuel-consumption rates vary according to the averaging time selected. The hourly emission rates consider operation of the equipment over the 1-, 3-, or 8-hr periods. For daily averaging times, the diesel-fueled engines are assumed to run for one shift per day (that is, one-third of a day). Therefore, the emission rates averaged over a day (24 hr) are one-third of the hourly rate. For the propane-fueled leachate treatment equipment that would be operated 24 hr/day, the hourly and daily fuel consumption rates are the same because they run full time, not just one-third of a day as with the diesel engines. Most operations do not occur over the full year. Therefore, the emission rate for annual averaging times was adjusted to the average over a year. In situations in which the operation does in fact occur for a 1-yr period and daily operations are estimated from annual use, the assumption is that operations would occur 250 days/yr (5 days per week and 50 weeks per year).

For operational safety, diesel-fired backup generators would be located at some facilities, such as the T Plant. Pollutant emissions would occur during brief periods when the generators are fired up for testing and maintenance purposes. At Hanford, backup diesel-fired generators are routinely run only once per month for a period of about 30 minutes. As a result of the low frequency and short duration of backup generator operations, the maximum annual air quality impacts to the public from all Hanford Solid Waste program activities should not be affected by the limited testing of diesel-fired generators. Flexibility in scheduling the operation of the generators would prevent emissions from occurring during periods with unfavorable dispersion conditions. As a result, the diesel-fired backup generators would not be in operation under conditions when emissions from other pollutant sources would produce the program's maximum 1-, 3-, 8-, and 24-hr air quality impacts to the public.

E.2 Fugitive Dust

Fugitive dust would be generated during Hanford solid waste activities as a result of various earthmoving activities and truck traffic. The release rate of particulates (with aerodynamic diameters of $30~\mu m$ or less) for earthmoving was estimated as $0.27~kg/(m^2-month)$ (EPA 1995a). This particulate emission rate was based on measurements made during the construction of apartments and shopping centers. The characteristics of the soil in this study are similar to soil conditions found in the 200 Areas. Assuming that the construction activities generating this level of particulate emissions were active 8~hr/day and 30~days/month, the particulate emission rate would amount to $3.1E-4~g/(m^2-s)$.

 Much of the fugitive dust generated by construction activities would be at the larger end of the 30- μ m range and would tend to settle rapidly (Seinfeld 1986). Experiments on dust suspension due to construction found that at 50 m (160 ft) downwind of the source, a maximum of 30 percent of the remaining suspended particulates at respirable height were in the PM₁₀ range (Grelinger et al. 1988). Based on this factor, only 30 percent of the total suspended particulates were assumed to be emitted as PM₁₀.

Activity ^(a) Diesel-Fuel Construction South Construction Constructi			Operation/		Fuel Consump	tion Rate for	· Indicated	
Activity ⁶⁰ Use (Liters) Time Note Hourly Daily Annual								
LLW Construction	Activity ^(a)	Use (Liters)		Note				
Alt. Group B - H & L 164,000 40 d 3 trenches	LLW Construction				·	·		
Alt. Group B - H & L Alt. Group B - U 275,000 Alt. Group C - H & L 110,000 Alt. Group C - H & L 110,000 Alt. Group C - H & L 110,000 Alt. Group C - U 110,000 Alt. Group C - U 110,000 Alt. Group C - U 110,000 Alt. Group C - U 110,000 Alt. Group C - U 110,000 Alt. Group C - U 110,000 Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group A - U Alt. Group B - H & L 300,000 28 wk 3x.1.25 ha trench 0.056 0.019 0.0035 0.0035 0.0036 0.0093 0.0063 0.0063 0.0063 0.13(c) 0.0095 0.0095 0.0095 0.0095 0.0095 0.0096 0.019 0.013 0.0063 0.13(c) 0.0096 0.0095 0.0095 0.0096 0.0096 0.0096 0.0096 0.0098 0.0093 0.0063 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0096 0.0098 0.0093 0.0063	Alt. Group A – H & L	110,000	40 d	1 trench	0.095	0.032	0.0035	
Alt. Group B - H & L Alt. Group B - U 275,000 40 d 5 trenches (b) Alt. Group C - H & L 110,000 40 d 1 trench 0.095 0.032 0.0035 Alt. Group C - H & L 110,000 40 d 1 trench 0.095 0.032 0.0035 Alt. Group C - U 110,000 40 d 1 trench 0.095 0.032 0.0035 Alt. Group C - H & L 110,000 40 d 1 trench 0.095 0.032 0.0035 Alt. Group A - H & L 200,000 1 yr 1.5 ha trench 0.028 0.0093 0.0063 Alt. Group A - H & L 300,000 28 wk 3x.1.25 ha trench 0.05(c) 0.086 0.099 0.0093 0.0063 Alt. Group B - H & L 300,000 28 wk 3x.1.25 ha trench 0.026 0.086 0.099 0.013 0.0063 0.0063 0.014 Alt. Group C - H & L 200,000 1 yr 2x.1.25 ha trench 0.028 0.0093 0.0063 0.0063 0.013(c) 0.014 Alt. Group C - H & L 200,000 1 yr - 0.028 0.0093 0.0095 0.036(c) 0.038(c) 0.0033 0.0063 Alt. Group C - H & L 200,000 1 yr - 0.028 0.0093 0.0063 0.0063 0.0063 0.0095 0.0032 0.0095 0.0035 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0095 0.0096 0.0098 0.0097 0.0048 0.0098 0.0093 0.0063 0.0093 0.0063 0.0093 0.0063 0.0096 0.0098 0.0093 0.0063 0.0096 0.0098 0.0093 0.0093 0.0063 0.0096 0.0098 0.0093 0.0063 0.0095 0.0098 0.0093 0.0093 0.0063 0.0095 0.0098 0.0093 0.0093 0.0063 0.0095 0.0098 0.0099 0.013 0.0048 0.0099 0.013 0.0042(c) 0.0048(c) 0.0042(c) 0.0048(c) 0.0042(c) 0.	Alt. Group A – U	110,000	40 d	1 trench	0.095	0.032	0.0035	
Alt. Group C – H & L			40 d	3 trenches ^(b)				
Alt. Group C – H & L 110,000 40 d 1 trench 0.095 0.032 0.0035 No Action 164,000 40 d 1 trench 0.095 0.032 0.0035 No Action 164,000 40 d 1 trench 0.095 0.032 0.0035 MLLW Construction Alt. Group A – H & L 200,000 1 yr 1.5 ha trench 0.028 0.0093 0.0063 Alt. Group B – H & L 300,000 28 wk 2x1.25 ha trench 0.056 0.019 0.013 Alt. Group B – H & L 200,000 1 yr - 0.0052 0.084 0.0095 Alt. Group B – U 450,000 28 wk 3x1.25 ha trench 0.028 0.0093 0.0063 Alt. Group C – H & L 200,000 1 yr - 0.028 0.0093 0.0063 Alt. Group C – H & L 200,000 1 yr - 0.028 0.0093 0.0063 Alt. Group C – H & L 200,000 1 yr - 0.028 0.0093 0.0063 Alt. Group D – H & L 7,760,000 2 yr (d) 0.54 0.18 0.12 Alt. Group D – H & L 7,760,000 2 yr (d) 0.55 0.18 0.12 Alt. Group D – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E – H & L 420,000 1 yr (e) 0.055 0.18 0.13 Alt. Group E – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E – H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group B – H & L 420,000 1 yr (e) 0.058 0.009 0.027 Melter & ILAW Construction 0.0000000000000000000000000000000000		275,000	40 d	5 trenches ^(b)	0.24	0.080	0.0087	
Alt. Group A - U		110,000	40 d	1 trench	0.095	0.032	0.0035	
No Action		110,000	40 d	1 trench	0.095	0.032	0.0035	
MLL W Construction Alt. Group A - H & L 200,000 1 yr 3.0 ha trench 0.028 0.0093 0.0063 Alt. Group A - U 400,000 1 yr 3.0 ha trench 0.056 0.019 0.013 Alt. Group B - H & L 300,000 28 wk 3x1.25 ha trench 0.056 0.019 0.013 Alt. Group B - U 450,000 28 wk 3x1.25 ha trench 0.056 0.019 0.014 Alt. Group C - H & L 200,000 1 yr - 0.056 0.019 0.013 Alt. Group C - U 400,000 1 yr - 0.056 0.019 0.013 Alt. Group C - U 400,000 1 yr - 0.056 0.019 0.013 Alt. Group D - H & L 7,760,000 2 yr (d) 0.54 0.18 0.12 Alt. Group D - H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group D - H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E - H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E - H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E - H & L 420,000 1 yr (e) 0.058 0.019 0.013 Alt. Group E - U 840,000 1 yr (e) 0.12 0.039 0.027 Alt. Group B - H & L 450,000 2 yr (6 vaults/yr 0.49 0.16 0.11 1.14	No Action	164,000	40 d	3 trenches ^(b)	0.14	0.047	0.0052	
Alt. Group A – U	MLLW Construction	,						
Alt. Group A — U	Alt. Group A – H & L	200,000	1 yr	1.5 ha trench	0.028	0.0093	0.0063	
Alt. Group B - H & L				3.0 ha trench	0.056	0.019	0.013	
Alt. Group B – U							0.0095	
Alt. Group C - H & L								
Alt. Group C - U			1 vr	_				
No Action				_			0.013	
Mit. Group D - H & L 7,760,000 2 yr (d) 0.54 0.18 0.12	No Action			1 trench	0.13 ^(c)	0.042 ^(c)		
Alt. Group D - H & L	LMF Construction	,						
Alt. Group D - U 7,960,000 2 yr (d) 0.55 0.18 0.13 Alt. Group E - H & L 420,000 1 yr (e) 0.058 0.019 0.039 Melter & H.AW Construction Melter Trench 450,000 40 wk 1 trench 0.49 0.16 0.11 ILAW Trench 7,000,000 2 yr 6 vaults/yr 0.49 0.16 0.11 ILAW Vault 582,000 1 yr 0.081 0.027 0.018 CWC Construction No Action - per building No Action - melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.00078 LLBG Capping Alt. Group A - H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.029 MILW Capping B - H & L 109,440 3 wk 2x1.25ha trench 0.13 0.042 0.0087 Alt. Group B - U 109,440 3 wk 2x1.25ha trench 0.13 0.042 0.0085 Alt. Group C - U 273,600 15 wk - 0.13 0.042 0.0035 Alt. Group C - U 273,600 15 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0047 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 LLW Backfilling Alt. Group A - H & L 820 1 yr - 0.032 0.016 0.0053 0.00026 Alt. Group A - H & L 820 1 yr - 0.032 0.011 0.0053 0.00026 Alt. Group A - H & L 36,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 366,600,000 1 yr - 0.032 0.011 0.002 0.0017 Alt. Group A - H & L 820 1 yr - 0.032 0.011 0.00036 0.00026 Alt. Group A - H & L 820 1 yr - 0.032 0.011 0.00036 0.00026 Alt. Group B - H & L 820 1 yr - 0.032 0.011 0.00036 0.000026 Alt. Group B - H & L 820 1 yr - 0.032 0.011 0.00010 Alt. Group B - H & L 6,780 1 yr 3 trenches 0.048 0.0048 0.0016 0.00021		7,760,000	2 yr	(d)	0.54	0.18	0.12	
Alt. Group E - H & L					0.55		0.13	
Alt. Group E – U 840,000 1 yr (e) 0.12 0.039 0.027 Melter & ILAW Construction Melter Trench 450,000 40 wk 1 trench(f) 0.31(c) 0.042(c) 0.014 ILAW Trench 7,000,000 2 yr 6 vaults/yr 0.49 0.16 0.11 ILAW Vault 582,000 1 yr 0.081 0.027 0.018 CWC Construction No Action – per building 10,600(g) 120 d/bldg 8 bldg/y (2008) 0.017 0.0057 0.00078 LLBG Capping All Action Alternatives (h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping(c) Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench 0.13 0.042 0.0035 Alt. Group C – H & L 145,920 8 wk 2x1.25ha trench 0.13 0.042 0.0035 Alt. Group C – H & L 145,920 8 wk 2x1.25ha trench 0.13 0.042 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0035 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0046 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 3.64,800 20 wk 2018 0.13 0.042 0.0017 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.0053(0) 0.00001 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter 0.0016(0) 0.00010 Melter		, , , , , , , , , , , , , , , , , , ,	_		0.058	0.019		
Melter & ILAW Construction 450,000 40 wk 1 trench ^(f) 0.31 ^(c) 0.042 ^(c) 0.014 ILAW Trench 7,000,000 2 yr 6 vaults/yr 0.49 0.16 0.11 ILAW Vault 582,000 1 yr 0.081 0.027 0.018 CWC Construction 10,600 ^(g) 120 d/bldg 4 bldgs ^(b) & 0.012 ^(b) 0.0041 ^(b) 0.0027 ^(b) No Action – per building 10,600 ^(g) 120 d/bldg 4 bldgs ^(b) & 0.012 ^(b) 0.0041 ^(b) 0.0027 ^(b) No Action – melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.0007 ^(b) LLBG Capping All Action Alternatives ^(h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping ^(c) All. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0046 Alt. Group A – U 273,600 15 wk 3 ha trench 0.13 0.042 0.0087 Alt. Group C – H & L 145,920 8 wk - 0.13 0.0		,						
Melter Trench 450,000 40 wk 1 trench ^(f) 0.31 ^(c) 0.042 ^(c) 0.014 ILAW Trench 7,000,000 2 yr 6 vaults/yr 0.49 0.16 0.11 ILAW Vault 582,000 1 yr 0.081 0.027 0.018 CWC Construction No Action – per building 10,600 ^(g) 120 d/bldg 4 bldgs ^(b) & 0.012 ^(b) 0.0041 ^(b) 0.0027 ^(b) No Action – melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.00078 LBG Capping <td a="" color="" color<="" complex="" of="" rows="" td="" the=""><td></td><td>,</td><td>,</td><td></td><td></td><td></td><td></td></td>	<td></td> <td>,</td> <td>,</td> <td></td> <td></td> <td></td> <td></td>		,	,				
ILAW Trench 7,000,000 2 yr 6 vaults/yr 0.49 0.16 0.027 0.018	Melter Trench	450.000	40 wk	1 trench ^(f)	0.31 ^(c)	0.042 ^(c)	0.014	
ILAW Vault	ILAW Trench		2 vr			0.16		
CWC Construction 10,600(g) 120 d/bldg 4 bldgs(b) & 8 bldg/y (2008) 0.012(b) 0.0041(b) 0.0027(b) No Action – melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.00078 LLBG Capping All Action Alternatives(h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping(h) Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0046 Alt. Group A – U 273,600 15 wk 3 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench(b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0046 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter 364,800 20 wk 2018	ILAW Vault	, ,		- · · · · · · · · · · · · · · · · · · ·	0.081	0.027	0.018	
No Action – per building No Action – per building No Action – melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.00078 LLBG Capping All Action Alternatives (h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0087 Alt. Group A – U 273,600 15 wk 3 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench (b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk 2x1.25ha trench (b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0087 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Trenches 2,520,000 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group A – H & L 820 1 yr - 0.016 0.0032 0.0016 0.00021 Alt. Group B – H & L 820 1 yr - 0.016 0.0032 0.0016 0.00021 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group A – H & L 820 1 yr - 0.000026 Alt. Group A – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026 Alt. Group B – H & L 820 1 yr - 0.000026	CWC Construction	,						
No Action – melter pad 24,600 50 d 8 bldg/y (2008) 0.017 0.0057 0.00078 LLBG Capping All Action Alternatives (h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping (c) Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench (b) 0.25 0.084 0.0035 Alt. Group B – U 109,440 3 wk 2x1.25ha trench (b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0046 Alt. Group C – U 273,600 15 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 ILAW Trenches 2,520,000 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group A – H & L 820 1 yr - 0.016 0.0026 0.0016 0.00021 Alt. Group B – H & L 820 1 yr - 0.032 0.0016 0.00026 Alt. Group B – H & L 820 1 yr - 0.032 0.0016 0.00026 Alt. Group B – H & L 820 1 yr - 0.032 0.0016 0.000026 Alt. Group B – H & L 820 1 yr - 0.032 0.0016 0.000026 Alt. Group B – H & L 820 1 yr - 0.032 0.0016 0.000026 Alt. Group B – H & L 820 1 yr - 0.036 0.0016 0.000026		10.600 ^(g)	120 d/bldg	4 bldgs ^(b) &	0.012 ^(b)	0.0041 ^(b)	0.0027 ^(b)	
LLBG Capping		,						
All Action Alternatives ^(h) 912,000 1 yr 2046-2049 0.13 0.042 0.029 MLLW Capping ^(c) Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group B – U 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0046 Alt. Group C – U 273,600 15 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 LLW Backfilling Alt. Group A – H & L 820 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group B – H & L 820 1 yr - 0.016 ⁽ⁱ⁾ 0.0053 ⁽ⁱ⁾ 0.000026 Alt. Group B – H & L 820 1 yr - 0.032 ^(j) 0.011 ^(j) 0.00010 Alt. Group B – H & L 6,780 1 yr 3 trenches ^(b) 0.048 ⁽ⁱ⁾ 0.006 ⁽ⁱ⁾ 0.00021		,						
MLLW Capping ^(c) Alt. Group A – H & L 145,920 8 wk 1.5 ha trench 0.13 0.042 0.0046 Alt. Group A – U 273,600 15 wk 3 ha trench 0.13 0.042 0.0087 Alt. Group B – H & L 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group B – U 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group C – H & L 145,920 8 wk - 0.13 0.042 0.0046 Alt. Group C – U 273,600 15 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0087 Melter and ILAW Capping Melter and ILAW Capping Melter and ILAW Capping Melter and ILAW Capping 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.35 0.12 0.080 ILW Backfilling Alt. Group A – H & L 8		912.000	1 vr	2046-2049	0.13	0.042	0.029	
Alt. Group A – H & L Alt. Group A – U Alt. Group A – U Alt. Group B – H & L Alt. Group B – H & L Alt. Group B – H & L Alt. Group B – H & L Alt. Group B – U Alt. Group B – U Alt. Group B – U Alt. Group C – H & L Alt. Group C – U Alt. G	MLLW Capping ^(c)	,	,					
Alt. Group A - U 273,600 15 wk 3 ha trench 0.13 0.042 0.0087 Alt. Group B - H & L 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group B - U 109,440 3 wk 2x1.25ha trench ^(b) 0.25 0.084 0.0035 Alt. Group C - H & L 145,920 8 wk - 0.13 0.042 0.0046 Alt. Group C - U 273,600 15 wk - 0.13 0.042 0.0087 No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0017 Melter and ILAW Capping Melter 364,800 20 wk 2018 0.13 0.042 0.0017 ILAW Trenches 2,520,000 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group A - H & L 820 1 yr - 0.016 ⁽ⁱ⁾ 0.0053 ⁽ⁱ⁾ 0.000026 Alt. Group B - H & L 6,780 1 yr 3 trenches ^(b) 0.048 ⁽ⁱ⁾ 0.016 ⁽ⁱ⁾ 0.0016 ⁽ⁱ⁾ 0.00021		145,920	8 wk	1.5 ha trench	0.13	0.042	0.0046	
Alt. Group B – H & L			15 wk	3 ha trench	0.13		0.0087	
Alt. Group B - U			3 wk	2x1.25ha trench ^(b)	0.25		0.0035	
Alt. Group C - H & L			3 wk				0.0035	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			8 wk	-	0.13	0.042	0.0046	
No Action 54,720 3 wk 1.25 ha trench 0.13 0.042 0.0017 Melter and ILAW Capping 364,800 20 wk 2018 0.13 0.042 0.012 ILAW Trenches 2,520,000 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group A - H & L 820 1 yr - 0.016 ⁽ⁱ⁾ 0.0053 ⁽ⁱ⁾ 0.000026 Alt. Group A - U 3,210 1 yr - 0.032 ⁽ⁱ⁾ 0.011 ⁽ⁱ⁾ 0.00010 Alt. Group B - H & L 6,780 1 yr 3 trenches ^(b) 0.048 ⁽ⁱ⁾ 0.016 ⁽ⁱ⁾ 0.00021		273,600	15 wk	_	0.13	0.042	0.0087	
Melter and ILAW Capping 364,800 20 wk 2018 0.13 0.042 0.012 ILAW Trenches 2,520,000 1 yr - 0.35 0.12 0.080 ILAW Vault 6,600,000 1 yr - 0.92 0.31 0.21 LLW Backfilling Alt. Group A - H & L 820 1 yr - 0.016 ⁽ⁱ⁾ 0.0053 ⁽ⁱ⁾ 0.000026 Alt. Group A - U 3,210 1 yr - 0.032 ⁽ⁱ⁾ 0.011 ⁽ⁱ⁾ 0.00010 Alt. Group B - H & L 6,780 1 yr 3 trenches ^(b) 0.048 ⁽ⁱ⁾ 0.016 ⁽ⁱ⁾ 0.00021	1		3 wk	1.25 ha trench				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Melter	364,800	20 wk	2018	0.13	0.042	0.012	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ILAW Trenches			-				
LLW Backfilling Alt. Group A – H & L 820 1 yr - $0.016^{(i)}$ $0.0053^{(i)}$ 0.000026 Alt. Group A – U 3,210 1 yr - $0.032^{(j)}$ $0.011^{(j)}$ 0.00010 Alt. Group B – H & L 6,780 1 yr 3 trenches (b) $0.048^{(i)}$ $0.016^{(i)}$ 0.00021	ILAW Vault		_	-				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$,,	,			-		
Alt. Group A – U 3,210 1 yr $-$ 0.002 $^{(j)}$ 0.011 $^{(j)}$ 0.00010 Alt. Group B – H & L 6,780 1 yr 3 trenches $^{(b)}$ 0.048 $^{(i)}$ 0.048 $^{(i)}$ 0.00021		820	1 yr	_	$0.016^{(i)}$	0.0053 ⁽ⁱ⁾	0.000026	
Alt. Group B – H & L $6,780$ 1 yr 3 trenches ^(b) 0.048 ⁽ⁱ⁾ 0.016 ⁽ⁱ⁾ 0.00021				_				
				3 trenches ^(b)	$0.048^{(i)}$			
י די דון סטטובן בי בי בי בי בי בי בי בי בי בי בי בי בי	Alt. Group B – U	11,300	1 yr	5 trenches ^(b)	$0.079^{(i)}$	0.026 ⁽ⁱ⁾	0.00036	

- (a) Waste volume considered Hanford Only (H), Lower Bound (L), and Upper Bound (U) waste volumes.
- (b) Simultaneous construction/activity assumed.
- (c) Assumed maximum of eight trucks operating on each trench at one time, except for ILAW capping.
- (d) The sum of diesel used for LLW(Alt A), MLLW(Alt A), Melter, and ILAW trenches construction.
- (e) The sum of diesel used for Alternative A LLW and MLLW trenches construction.(f) Assumed consumption for each multiple trench design and for two modules of the single ILAW trench design.
- (g) Diesel required per building.
- (h) Applies to the LMF under Alternatives D and E.
- (i) Assumed maximum of one truck operating on each trench at a time.
- (j) Assumed maximum of two trucks operating on each trench at a time.
- (k) Other years Alternative A–L: 1000 L/yr 1999-2005 and 1200 L/yr 2008–2046.
- (1) Other years Alternative A–U: 1100 L/yr 1999-2004 and 2300 L/yr 2005–2046.
- (m) Assumed 6800 L/yr to backfill one current-design trench in one year.
- (n) Other year No Action: 1000 L/yr 2000-2006.
- (o) Melter trench backfilling could occur over 15 campaigns or all-at-once. All-at-once was assumed for conservatism (that is, highest emission rate of pollutants).
- CWC = Central Waste Complex.
- ILAW =immobilized low-activity waste.
- LLBG = low-level burial ground
- LLW = low-level waste.
- LMF = Lined Modular Facility.
- MLLW = mixed low-level waste.
- NWPF = new waste processing facility
- Source: FH 2003.

Operation/	Maximum	Operation/			onsumption	
Alternative (a)	Propane Use	Time of	Note (b)			Time (gal/s)
. ,	Propane Use	Maximum Use	Note (b)	Hourly	Daily	Annual
MLLW Leachate	(-)					
Pulse Drier	Ton/yr ^(c)					
Alt. Group A – H & L	330	36 d/yr	50 hr/campaign	0.091	0.091	0.0043
Alt. Group A – U	700	71 d/yr	96 hr/campaign	0.19	0.19	0.0091
Alt. Group B – H & L	2650	1 yr	2027; 32 hr/camp per tr	0.067	0.067	0.034
Alt. Group B – U	4505	1 yr	2032; 32 hr/camp per tr	0.13	0.13	0.059
Alt. Group C – H & L	330	36 d/yr	50 hr/campaign	0.091	0.091	0.0043
Alt. Group C – U	700	71 d/yr	96 hr/campaign	0.19	0.19	0.0091
Alt. Group D – H & L	770	78 d/yr	(d)	0.14	0.047	0.010
Alt. Group D – U	1140	113 d/yr	(d)	0.14	0.048	0.015
Alt. Group E – H & L	330	36 d/yr	50 hr/campaign	0.091	0.091	0.0043
Alt. Group E – U	700	71 d/yr	96 hr/campaign	0.19	0.19	0.0091
No Action	530	1 yr	2026-37; 32 hr/camp	0.067	0.067	0.0069
Melter Leachate/Pulse						
Drier						
Melter	440	42 d/yr	60 hr/campaign	0.13	0.13	0.0057
CWC Vehicles	Liter/yr(e)					
Alt. Group A – H & L	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group A – U	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group B – H & L	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group B – U	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group C – H & L	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group C – U	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group D – H & L	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group D – U	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group E – H & L	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
Alt. Group E – U	7600	1 yr	Max year 2002	0.00028	0.000093	0.000064
No Action – H & L	32400	1 yr	Max 2014-47	0.0012	0.00040	0.00027

- (a) Waste volume considered Hanford Only (H), Lower Bound (L), and Upper Bound (U) waste volumes.
- (b) All campaigns are assumed to be carried out in series over the year, except for Alternative B-U where two campaigns are assumed to occur at a time for hourly and daily fuel-consumption-rate calculations.
- (c) Conversion factor for propane = 409.8 gal/ton (Lide 2001).
- (d) The sum of propane use for Alternative A and melter.
- (e) Conversion factor 1 liter = 0.265 gallons.

Camp per tr = campaign per trench.

CWC = Central Waste Complex.

MLLW = mixed low-level waste.

Source: FH 2003.

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All Hanford Solid Waste Program activities would be conducted using dust-suppression techniques; however, no credit is taken for any reduction in PM_{10} emissions as a result of dust-suppression. Dust control during large earthmoving activities would comply with nuisance-dust-emission control requirements. Earthmoving activities would be restricted on days with excessive wind speeds. The use of dust-suppression methods would depend on the soil being excavated, wind speed, and visual observations. Water sprays for dust suppression were found to be very effective in controlling PM_{10} emissions at the Hanford Site (DOE-RL 1996). Monitoring of the effectiveness of water sprays found air-particulate concentrations at the location of earthmoving activity to be under 90 μ g/m³ (DOE-RL 1996), well within the 24-hr ambient air quality standard for PM_{10} of 150 μ g/m³. Most values were even lower.

Although not governed by ambient air quality standards, a potential concern for public safety is a short-term, wind-blown dust event at the borrow pit that could limit visibility on SR 240 and cause problems for passing motorists. To guard against this, an aggressive dust-suppression program is planned for this area. This dust-control program would include the following as needed:

• spraying of active work areas with water and a soil adhesive

• rocking of 8 km (5 mi) of project roads and periodic spray with solid adhesive

• covering of materials in truck beds with rollout tarps prior to transport

• other dust-suppression activities would also be considered for implementation when wind speeds are projected to exceed the threshold for significant dust generation.

The estimation of the annual and 24-hr average PM₁₀ emission values from earthmoving operations requires an estimate of the area being disturbed by earthmoving equipment. Estimates of the amount of area that would be disturbed by earthmoving activities are presented in Table E.12. The actual area that is actively being disturbed at any given time is estimated on a case-by-case basis. In general, for work sites where operation/construction times exceed a year, 2 percent of the annual disturbed area is assumed to be active at any one time. Work sites where the soil is actively disturbed for shorter periods of time have a correspondingly larger percentage of their total area being disturbed at any given time. For example, consider the 2.2 ha (5.4 ac) that would be disturbed over a period of 40 days for LLW construction activities under Alternative Group A. It was assumed that 2200 m² (2630 yd²), about 10 percent of the total disturbed area, would be actively disturbed at any given moment during this construction activity. Estimates of fugitive dust from material stockpiles are conservatively determined by assuming that the entire stockpile, or an appropriate portion of the stockpile based on its size, is an active construction site.

E.3 Calculating Maximum Air Quality Impacts

The maximum air quality impacts associated with each major project activity were calculated by putting together previous information, including unit dispersion factors (from ISCST3 model runs), fuel-consumption rates, size of disturbed areas, and emission factors. Table E.13 provides the maximum air quality impacts to the public for activities conducted in the 200 Areas under the assumptions noted for each activity in Tables E.10 and E.11. Construction and capping operations at the trenches (LLW, MLLW, and ILAW) and the transportation of capping materials would be substantial sources of pollutants and major contributors to maximum air quality impacts. Table E.14 indicates the maximum air quality impacts to the public from activities in the 200 Area. Table E.15 presents comparable information for Area C activities. Looking at the individual pollutants:

• LLW and ILAW capping would be the largest contributors to PM₁₀ air quality impacts. The transportation of capping materials to the trenches and LMF, LLW, and ILAW construction would also represent substantial sources of PM₁₀.

• ILAW capping activities (particularly under the No Action Alternative) and LMF construction would produce the largest air quality impact for NO₂.

also represent substantial sources of SO₂ and CO.

• LMF construction and ILAW capping would generate the largest air quality impacts for SO₂ and CO.

LLW and MLLW construction and capping activities (particularly under Alternative Group B) would

Table E.12. The Size of Disturbed Areas and Associated Durations for Various Activities/Alternatives

	Cumulative	Duration of	Percentage of Total	Amount of Area Being
(0)	Disturbed Area	Operation/	Area Actively	Disturbed at Any Given
Activity ^(a)	(Hectares)	Construction (Time)	Disturbed	Time (m ²)
LLW Construction				
Alt. Group A – H & L	2.2	40 d	10	2200
Alt. Group A – U	2.2	40 d	10	2200
Alt. Group B – H & L	3 x 0.55	40 d	10	1650
Alt. Group B – U	5 x 0.55	40 d	10	2750
Alt. Group C – H & L	2.2	40 d	10	2200
Alt. Group C – U	2.2	40 d	10	2200
No Action	3 x 0.55	40 d	10	1650
MLLW Construction				
Alt. Group A – H & L	1.50	1 yr	2.0	300
Alt. Group A – U	3.00	1 yr	2.0	600
Alt. Group B – H & L	2 x 0.60	28 wk	3.6	430
Alt. Group B – U	3 x 0.60	28 wk	3.6	640
Alt. Group C – H & L	1.50	1 yr	2.0	300
Alt. Group C – U	3.00	1 yr	2.0	600
No Action	0.60	28 wk	3.3	200
LMF Construction ^(b)				
Alt. Group D – H & L	3.7	2 yr	6.3	2350
Alt. Group D – U	5.2	2 yr	4.8	2500
Alt. Group E – H & L	3.7	2 yr	6.3	2350
Alt. Group E – U	5.2	2 yr	4.8	2500
Melter Construction				
Melter trench	6.0 ^(c)	40 wk	2.5	1500
ILAW Construction				
Alt. Group A – ILAW Trench	26.0	15 yr	1.0	2600
Alt. Group B – ILAW Trench	26.0	15 yr	1.0	2600
Alt. Group C – ILAW Trench	8.0	15 yr	1.0	800
Alt. Group D – ILAW Trench	8.0	15 yr	1.0	800
Alt. Group E – ILAW Trench	8.0	15 yr	1.0	800
No Action – ILAW Vaults	10.0	15 yr	1.0	1000
CWC Construction				
No Action – per building	1.00	1 yr	5.	500
No Action – pad construction	0.100	50 d	20.	200
LLBG Capping				
All Action Alternatives	93.50	4 yr	0.50	4700

	Cumulative		Percentage of	Amount of Area		
	Disturbed Area	Duration of Operation/	Total Area	Being Disturbed at		
Activity ^(a)	(Hectares)	Construction (Time)		Any Given Time (m ²)		
MLLW Capping	(Hectares)	Constituction (Time)	Actively Disturbed	Any Given Time (m)		
Alt. Group A – H & L	1.50	8 wk	10	1500		
Alt. Group A – U	3.00	15 wk	5	1500		
Alt. Group B – H & L	2 x 0.60	3 wk	10	1200		
	2 x 0.60	3 wk	10	1200		
Alt. Group B – U		8 wk				
Alt. Group C – H & L	1.50	= ''	10	1500		
Alt. Group C – U	3.00	15 wk	5	1500		
Alt. Group D – H & L	1.50	8 wk	10	1500		
Alt. Group D – U	3.00	15 wk	5	1500		
Alt. Group E – H & L	1.50	8 wk	10	1500		
Alt. Group E – U	3.00	15 wk	5	1500		
No Action	0.60	3 wk	10	600		
Melter and ILAW Capping	İ					
Melter	6.0	20 wk	3	1800		
Alt. Group A – ILAW Trench	26.0	15 yr	1.0	2600		
Alt. Group B – ILAW Trench	26.0	15 yr	1.0	2600		
Alt. Group C – ILAW Trench	8.0	15 yr	1.0	800		
Alt. Group D – ILAW Trench	8.0	15 yr	1.0	800		
Alt. Group E – ILAW Trench	8.0	15 yr	1.0	800		
No Action – ILAW Vaults	10.0	15 yr	1.0	1000		
LLW Backfilling						
Alt. Group A – H & L	0.18	1 yr	2.0	40		
Alt. Group A – U	0.71	1 yr	2.0	140		
Alt. Group B – H & L	1.50	1 yr	2.0	300		
Alt. Group B – U	2.50	1 yr	2.0	500		
Alt. Group C – H & L	0.18	1 yr	2.0	40		
Alt. Group C – U	0.71	1 yr	2.0	140		
Alt. Group D – H & L	0.18	1 yr	2.0	40		
Alt. Group D – U	0.71	1 yr	2.0	140		
Alt. Group E – H & L	0.18	1 yr	2.0	40		
Alt. Group E – U	0.71	1 yr	2.0	140		
No Action	1.50	1 yr	2.0	300		
MLLW Backfilling ^(d)		,				
Alt. Group A – H & L	0.15 max	1 yr	2.0	30		
Alt. Group A – U	0.30 max	1 yr	2.0	60		
Alt. Group B – H & L	0.60 max	1 yr	2.0	120		
Alt. Group B – U	1.20 max	1 yr	2.0	240		
Alt. Group C – H & L	0.15 max	1 yr	2.0	30		
Alt. Group C – U	0.30 max	1 yr	2.0	60		
Alt. Group D – H & L	0.15 max	1 yr	2.0	30		
Alt. Group D – II & L Alt. Group D – U	0.13 max 0.30 max	1 yr	2.0	60		
Alt. Group E – H & L	0.30 max 0.15 max		2.0	30		
	0.15 max 0.30 max	1 yr				
Alt. Group E – U	0.30 max 0.15 max	1 yr	2.0 2.0	60		
No Action Melter	$3.50^{(c)}$	1 yr 6 wk		30		
MICHEL	3.30	U WK	10	3500		

Activity ^(a)	Cumulative Disturbed Area (Hectares)	Duration of Operation/ Construction (Time)	Total Area	Amount of Area Being Disturbed at Any Given Time (m ²	
Treatment Facility	,		·	` ′	
T Plant Modification (Alt A,C,D,E)	3.50	4 yr	1.0	350	
NWPF Construction (Alt B)	3.50	4 yr	1.0	350	
Borrow Activity					
Borrow operations	81.0	12 yr	0.20	1600	

- (a) Waste volume considered Hanford Only (H), Lower Bound (L) and Upper Bound (U) waste volumes.
- (b) Without ILAW or melter construction portions.
- (c) Includes road construction.
- (d) Waste area only; all-at-once backfilling considered to maximize emission rate of particulates.

Source: FH 2003.

NWPF = new waste processing facility

	Maximum Air Quality Impacts (mg/m³) for the Indicated Averaging Periods (b)								
	PN	$I_{10}^{(c)}$		S	$\overline{\mathbf{O}_2}$	CC)	NO_2	
Activity ^(a)	24 hr	Annual	1 hr	3 hr	24 hr	Annual	1 hr	8 hr	Annual
LLW Construction									
Alt. Group A – H&L	12	0.013	12	5.8	0.42	4.3E-4	230	73	0.020
Alt. Group A – U	12	0.013	12	5.8	0.42	4.3E-4	230	73	0.020
Alt. Group B – H&L	11	0.011	18	8.5	0.62	6.4E-4	340	110	0.030
Alt. Group B – U	18	0.018	31	15	1.0	1.1E-3	580	180	0.051
Alt. Group C – H&L	12	0.013	12	5.8	0.42	4.3E-4	230	73	0.020
Alt. Group C – U	12	0.013	12	5.8	0.42	4.3E-4	230	73	0.020
No Action	11	0.011	18	8.5	0.62	6.4E-4	340	110	0.030
MLLW Construction									
Alt. Group A – H&L	2.0	0.017	3.7	1.7	0.12	7.7E-4	67	21	0.037
Alt. Group A – U	3.9	0.034	7.3	3.4	0.25	1.6E-3	130	43	0.076
Alt. Group B – H&L	6.8	0.015	33	15	1.1	1.2E-3	600	190	0.056
Alt. Group B – U	10	0.023	50	23	1.7	1.7E-3	910	290	0.082
Alt. Group C – H&L	1.1	0.010	1.9	0.76	0.071	4.6E-4	35	9.2	0.022
Alt. Group C – U	2.3	0.020	3.9	1.5	0.14	9.5E-4	71	18	0.045
No Action	3.3	0.0074	17	7.9	0.55	5.9E-4	310	99	0.028
LMF Construction									
Alt. Group D – H&L	11	0.070	71 ^(b)	33 ^(b)	2.4 ^(b)	0.015 ^(b)	1300 ^(b)	410 ^(b)	0.70
Alt. Group D – U	11	0.070	71 ^(b)	33 ^(b)	2.4 ^(b)	0.015 ^(b)	1300 ^(b)	410 ^(b)	0.70
Alt. Group E – H&L	1.8	0.014	7.6	3.5	0.25	1.6E-3	140	44	0.076
Alt. Group E – U	3.6	0.028	16	7.3	0.51	3.3E-3	290	92	0.16
Melter & ILAW									
Construction									
Melter Trench	5.6	0.035	21	8.4	0.32	1.0E-3	390	100	0.049
ILAW									
Alt. Groups A, B	21	0.17	64	30	2.1	0.014	1200	370	0.64
ILAW portions only									
Alt. Groups C, D, E	13	0.094	64	30	2.1	0.014	1200	370	0.64
ILAW No Action	3.7	0.032	5.6	2.2	0.21	1.3E-3	100	27	0.062
CWC Construction									
No Action – per bldg	2.6	0.024	1.6	0.73	0.054	3.3E-4	29	9.2	0.016
No Action – melter									
Pad	1.3	0.0016	2.2	1.0	0.075	9.6E-5	41	13	4.6E-3

NA = "Not Applicable" – There are no SO₂ emissions from the propane used for this activity.

⁽a) Waste volume considered – Hanford Only (H), Lower Bound (L) and Upper Bound (U) waste volumes.

⁽b) The maximum air quality impact is indicated with **bold text** for each averaging period.

⁽c) Includes both fugitive dust and diesel combustion particulates.

⁽d) See Low Level Burial Ground (LLBG) capping. Lined modular facility (LMF) capping occurs at same rate as the LLBG capping during the maximum year.

	Maximum Air Quality Impacts (mg/m³) for the Indicated Averaging Periods (b)								
		[10 ^(c)			$\overline{O_2}$	CC	NO ₂		
Activity ^(a)	24 hr	Annual	1 hr	3 hr	24 hr	Annual	1 hr	8 hr	Annual
Transporting									
Capping Materials									
All Alternatives	24	0.23 ^(b)	4.2	1.9	0.42	3.9E-3	130	42	0.081
LIBC Coming									
LLBG Capping All Action Alts	25 ^(b)	0.23 ^(b)	177	7.0	0.55	2.00.2	210	00	0.17
All Action Aits	25~	0.25	17	7.9	0.55	3.6E-3	310	99	0.17
MLLW Capping									
Alt. Group A – H&L	9.6	0.013	17	7.9	0.55	5.7E-4	310	99	0.027
Alt. Group A – U	9.6	0.024	17	7.9	0.55	1.1E-3	310	99	0.051
Alt. Group B – H&L	10	4.9E-3	33	15	1.1	4.3E-4	600	190	0.020
Alt. Group B – U	10	4.9E-3	33	15	1.1	4.3E-4	600	190	0.020
Alt. Group C – H&L	5.6	7.6E-3	9.0	3.5	0.32	3.4E-4	160	43	0.016
Alt. Group C – U	5.6	0.014	9.0	3.5	0.32	6.3E-4	160	43	0.030
No Action	3.0	1.5E-3	9.0	3.5	0.32	1.2E-4	160	43	5.9E-3
Melter & ILAW									
Capping									
Melter Trench	6.4	0.022	9.0	3.5	0.32	8.8E-4	160	43	0.042
ILAW									
Alt. Groups A, B	19	0.16	46	21	1.6	9.8E-3	840	270	0.47
ILAW	11	0.079	46	21	1.6	9.8E-3	840	270	0.47
Alt. Groups C, D, E ILAW No Action	13	0.078	63	25	1.6 2.4 ^(b)	9.8E-3 0.015 ^(b)	1200	300	0.47 0.73 ^(b)
ILAW NO ACTION	13	0.092	0.5	25	2.4	0.015	1200	300	0.75
LLW Backfilling									
Alt. Group A – H&L	0.49	1.8E-3	2.1	0.97	0.070	3.2E-6	38	12	1.5E-4
Alt. Group A – U	1.3	6.4E-3	4.2	1.9	0.14	1.2E-5	77	24	5.9E-4
Alt. Group B – H&L	2.3	0.014	6.3	2.9	0.21	2.6E-5	120	37	1.2E-3
Alt. Group B – U	3.9	0.023	10	4.8	0.34	4.4E-5	190	60	2.1E-3
Alt. Group C – H&L	0.49	1.8E-3	2.1	0.97	0.070	3.2E-6	38	12	1.5E-4
Alt. Group C – U	1.3	6.4E-3	4.2	1.9	0.14	1.2E-5	77	24	5.9E-4
Alt. Group D – H&L	1.4	3.0E-3	6.3	2.9	0.28	2.7E-4	120	37	0.013
Alt. Group D – U	2.2	7.6E-3	8.4	3.9	0.35	3.0E-4	150	49	0.014
Alt. Group E – H&L	0.49	1.8E-3	2.1	0.97	0.071	9.8E-6	38	12	4.7E-4
Alt. Group E – U	1.3	6.4E-3	4.2	1.9	0.16	2.6E-5	77	24	1.2E-3
No Action	1.4	8.1E-3	3.3	1.3	0.12	1.5E-5	120	16	7.3E-4

NA = "Not Applicable" – There are no SO_2 emissions from the propane used for this activity.

⁽a) Waste volume considered – Hanford Only (H), Lower Bound (L) and Upper Bound (U) waste volumes.

⁽b) The maximum air quality impact is indicated with **bold text** for each averaging period.

⁽c) Includes both fugitive dust and diesel combustion particulates.

d) See Low Level Burial Ground (LLBG) capping. Lined modular facility (LMF) capping occurs at same rate as the LLBG capping during the maximum year.

NA = "Not Applicable" – There are no SO₂ emissions from the propane used for this activity.

NA

1.1E-5

1.7E-3

NA

NA

NA

0.28

0.089

1.6E-3

No Action

⁽a) Waste volume considered – Hanford Only (H), Lower Bound (L) and Upper Bound (U) waste volumes.

⁽b) The maximum air quality impact is indicated with **bold text** for each averaging period.

⁽c) Includes both fugitive dust and diesel combustion particulates.

⁽d) See Low Level Burial Ground (LLBG) capping. Lined modular facility (LMF) capping occurs at same rate as the LLBG capping during the maximum year.

	P	PM_{10}		SO_2				CO	
	24 hr	Annual	1 hr	3 hr	24 hr	Annual	1 hr	8 hr	Annual
Ambient Air Quality Standard									
$(\mu g/m^3)$	150	50	1,000	1,300	260	50	40,000	10,000	100
Maximum Impact – single activity									
$(\mu g/m^3)$	25	0.23	71	33	2.4	0.015	1300	410	0.73
Maximum Impact – single activity									
(Percent of Standard)	17	0.46	7.1	2.5	0.92	0.030	3.2	4.1	0.73
Activity creating maximum impact ^(a)	a	a, d	b	b	b, c	b, c	b	b	c

Note: All alternatives are considered in selecting the activities with the maximum air quality impacts.

- (a) Activities creating maximum impacts:
 - a. LLBG capping
 - b. LMF trench construction
 - c. ILAW vault capping
 - d. Transportation of capping materials

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The maximum air quality impacts from all project emissions in the 200 Areas were obtained by combining the data in Table E.13 with the project-activity scheduling data presented in Tables E.3 through E.8. These estimates are presented in Table 5.4 and Tables 5.6 through 5.10 in Section 5.2.

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Operations at the borrow pit and the emissions from the transportation of capping materials are the two largest sources of pollutants in the vicinity of Area C. Both activities would generally occur simultaneously. The maximum air quality impacts from emissions in Area C were obtained by combining the data in Table E.15 with the project-activity scheduling data presented in Tables E.3 through E.8. These estimates are presented in Table 5.5 in Section 5.2.

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Table E.15. Maximum Air Quality Impacts to the Public from Activities with an Area C Source Location

	Maximum Air Quality Impacts (mg/m³) for the Indicated Averaging Periods								
	PI	M_{10}	SO_2				CO		NO ₂
Activity(a)	24 hr	Annual	1 hr	3 hr	24 hr	Annual	1 hr	8 hr	Annual
Utility Extensions									
All Alternatives	0.56	2.8E-4	130	96	0.13	6.5E-05	2300	1300	3.1E-03
Operations									
All Alternatives	5.6	0.049	180 ^(b)	140 ^(b)	0.18	1.1E-03	3300 ^(b)	1900 ^(b)	0.054 ^(b)
Propane Emissions									
All Alternatives	0.056	3.8E-04	-	-	-	-	320	180	0.052
Transportation of Capping Materials									
All Alternatives	15 ^(b)	0.14 ^(b)	85	65	0.26 ^(b)	2.4E-03 ^(b)	2700	1600	0.050

- (a) Waste volume considered Hanford Only (H), Lower Bound (L) and Upper Bound (U) waste volumes.
- (b) The maximum air quality impact is indicated with **bold text** for each averaging period.

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DOE guidance suggests a method to formally report how EIS actions relate to the Clean Air Act (CAA) (42 USC 7401), which implements General Conformity Requirements (DOE 2000). The CAA General Conformity Requirements method is, in general, another means to validate the acceptability of the release estimates resulting from an action. The guidance requires that a conformity review be conducted to determine if detailed analyses and reporting would be required for EIS actions to be conducted. It is intended to ensure that actions would not further impair or sustain current excesses of criteria pollutant levels. This review would allow faster implementation of the action once a record of decision or finding of no significant impact is issued. It is important to note that the emissions reported in a conformity review may be narrower than sources considered in an EIS air quality assessment (DOE 2000).

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Table E.16. Clean Air Act Conformity Review for the Alternatives

The conformity review process consists of answering four questions (see Table E.16). The DOE (2000) recommends that a conformity review be conducted for each EIS alternative. Normally, a

conformity review are presented in Table E.16. As a result of the conformity-review process, it has

conformity review is not needed for the No Action Alternative (DOE 2000). The results of the

been determined that a Conformity Determination need not be conducted.

	Question	All Alternative Groups
1.	Are criteria pollutants emitted?	Yes
2.	Would criteria pollutant emissions occur in a non-attainment or maintenance area?	No, the Hanford Site is an attainment area. (a)
3.	Is the action(s) exempt from the Clean Air Act Conformity Requirements?	No; therefore, the actions are not exempt outright from air quality requirements.
4.	What are the estimated emissions and how do they compare to the non-attainment (or maintenance) area threshold emission rates and emission inventory?	The Hanford Site is in an attainment area. Also, the estimated maximum releases do not exceed Clean Air Act Criteria Pollutant standards.
(a)	Ecology (2001).	•

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E.5 References

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